

ORBIT Room Radio Propagation Measurements

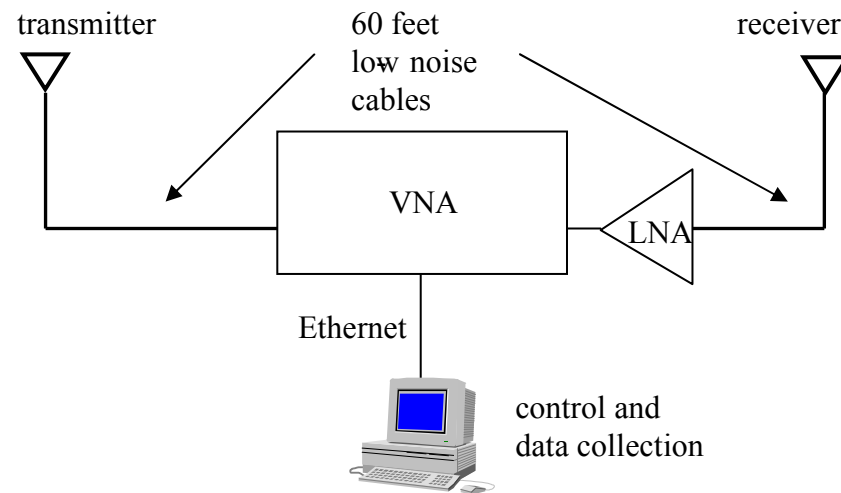
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Outline

- Measurements setup
 - network analyzer
 - signal generator and spectrum analyzer
- Measurements background
 - path loss
 - impulse response (multipath intensity profile)
- Two case studies
 - 15 measurements diagonally across the room
 - 66 measurements for two transmitter positions
 - impulse response compared to WISE prediction

Vector Network Analyzer

- measures s-parameters
- $J=1601$ tones in bandwidth
 - ISM/UNII 100 MHz bands
 - 2.4 to 2.5 GHz
 - 5.15 to 5.25 GHz
 - 5.25 to 5.35 GHz
 - 5.725 to 5.825 GHz
 - wide bandwidth W (coarse)
 - 0.4 to 6 GHz
 - maximum delay
 - multipath resolution

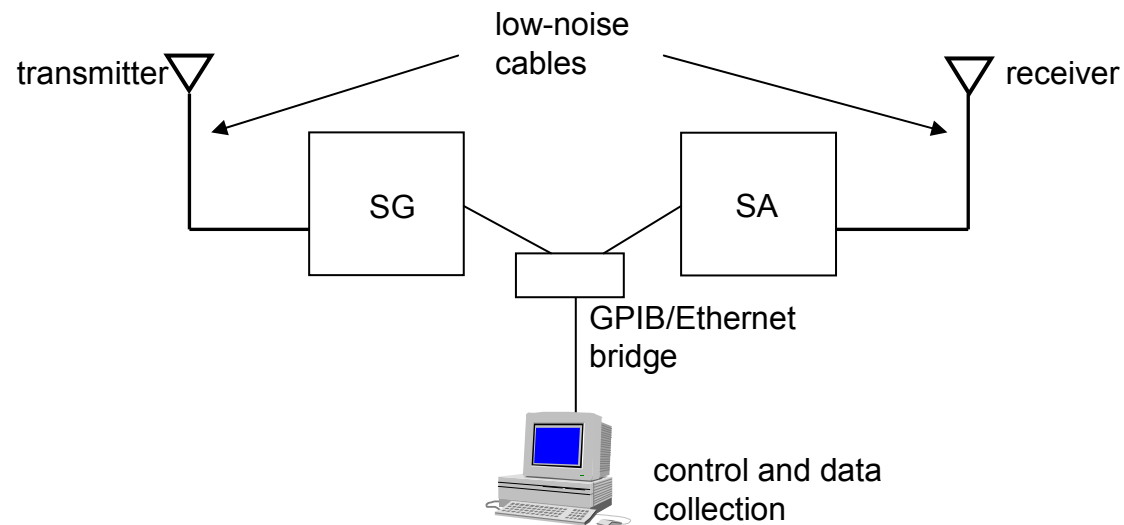


$$\tau_{\max} = \frac{J-1}{W} = \frac{1600}{(6-0.4) \cdot 10^9} = 286 \text{ ns} \Rightarrow 85.7 \text{ m}$$

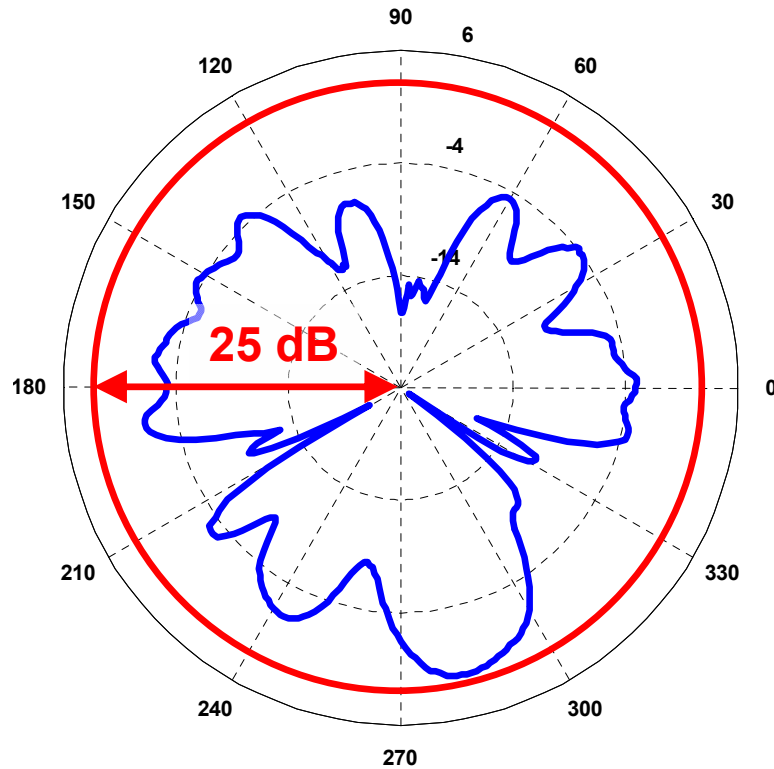
$$\Delta\tau = \frac{1}{W} = \frac{1}{(6-0.4) \cdot 10^9} = 179 \text{ ps} \Rightarrow 5.36 \text{ cm}$$

Signal generator and spectrum analyzer

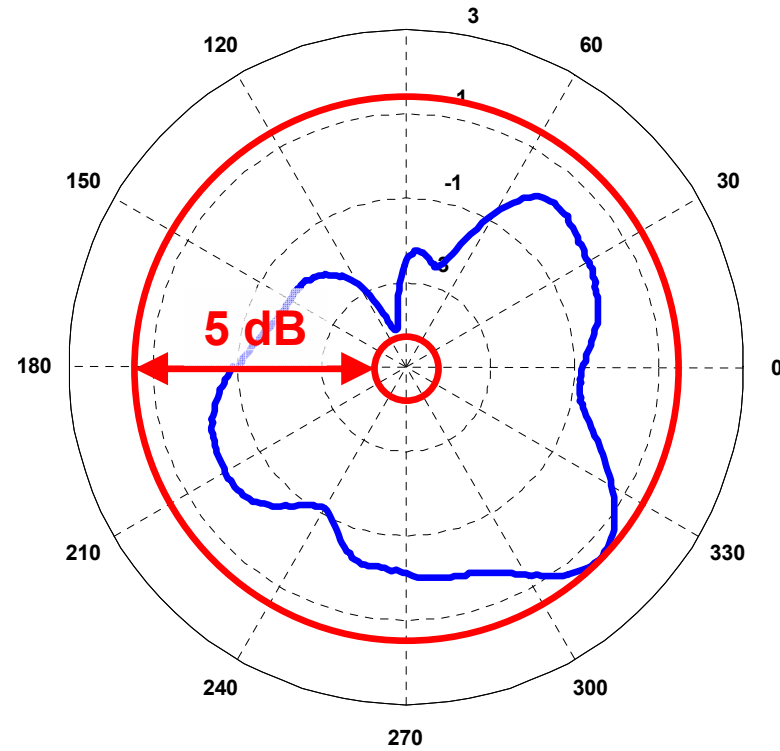
- measure power loss
- send J=51 tones across four ISM/UNII 100 MHz bands
- compare to and verify VNA measurements



Antenna patterns*



elevation



azimuth

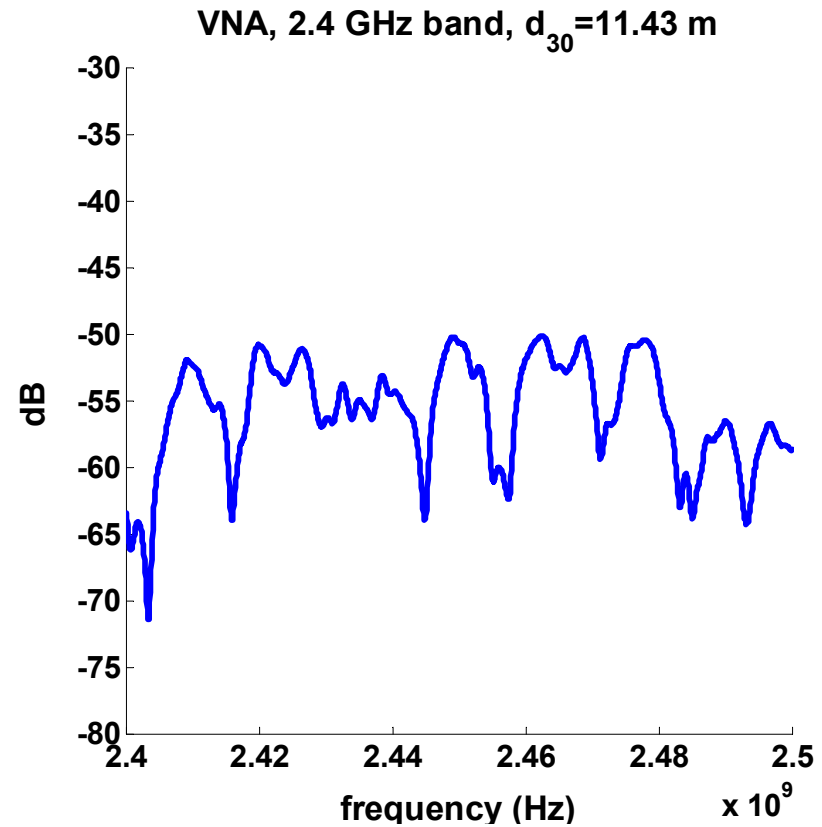
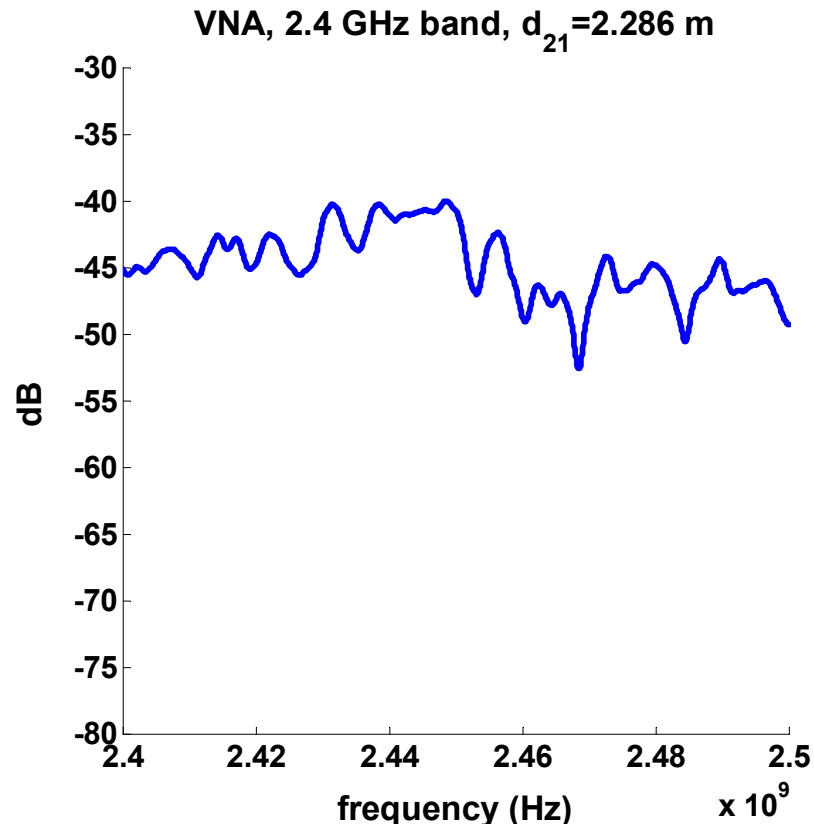
* Thanks to Ilya Korisch from Lucent in Holmdel

Path loss measurements reduction

- Channel response $H(f_j, d_k)$ (Ghassemzadeh et al. '03)
 - at frequency f_j $j=0,1,\dots,J-1$
 - at distance d_k $k=1,2,\dots,K$
 - average of ten measurements taken over two-minutes period
- Path loss at distance d_k averaged over J frequencies
 - $J=1601$ for VNA and $J=51$ for SG/SA

$$PL(d_k) = -10 \log_{10} \left(\frac{1}{J} \sum_{j=0}^{J-1} |H(f_j, d_k)|^2 \right)$$

Examples of channel response $H(f_j, d_k)$



Path loss best fit

- Assume path loss model

$$PL_{fit}(d) = PL_1 + 10\gamma \log_{10}\left(\frac{d}{d_1}\right)$$

- Perform nonlinear least squares fitting

$$\gamma^*, PL_1^* = \arg \min_{\gamma, PL_1} \left\{ \sum_{k=1}^K \left(PL(d_k) - PL_{fit}(d_k) \right)^2 \right\}$$

Impulse response

- Impulse response (Ghassemzadeh et al. '05)

$$g^k(\tau) = \sum_{j=0}^{J-1} a_j^k \delta(\tau - \tau_j)$$

$$\tau_j = j \cdot \Delta\tau$$

$$\{a_j^k\} = IDFT(H(f_j, d_k))$$

- Path gain

$$G_k = \sum_{j=0}^{J-1} |a_j^k|^2$$

Multipath intensity profile

- Delay profile

- normalized sum of powers of a_j^k

$$p^k(\tau) = \sum_{j=0}^{J-1} p_j^k \delta(\tau - \tau_j); \quad p_j^k = \frac{|a_j^k|^2}{G_k}$$

- Power-delay profile (PDP)

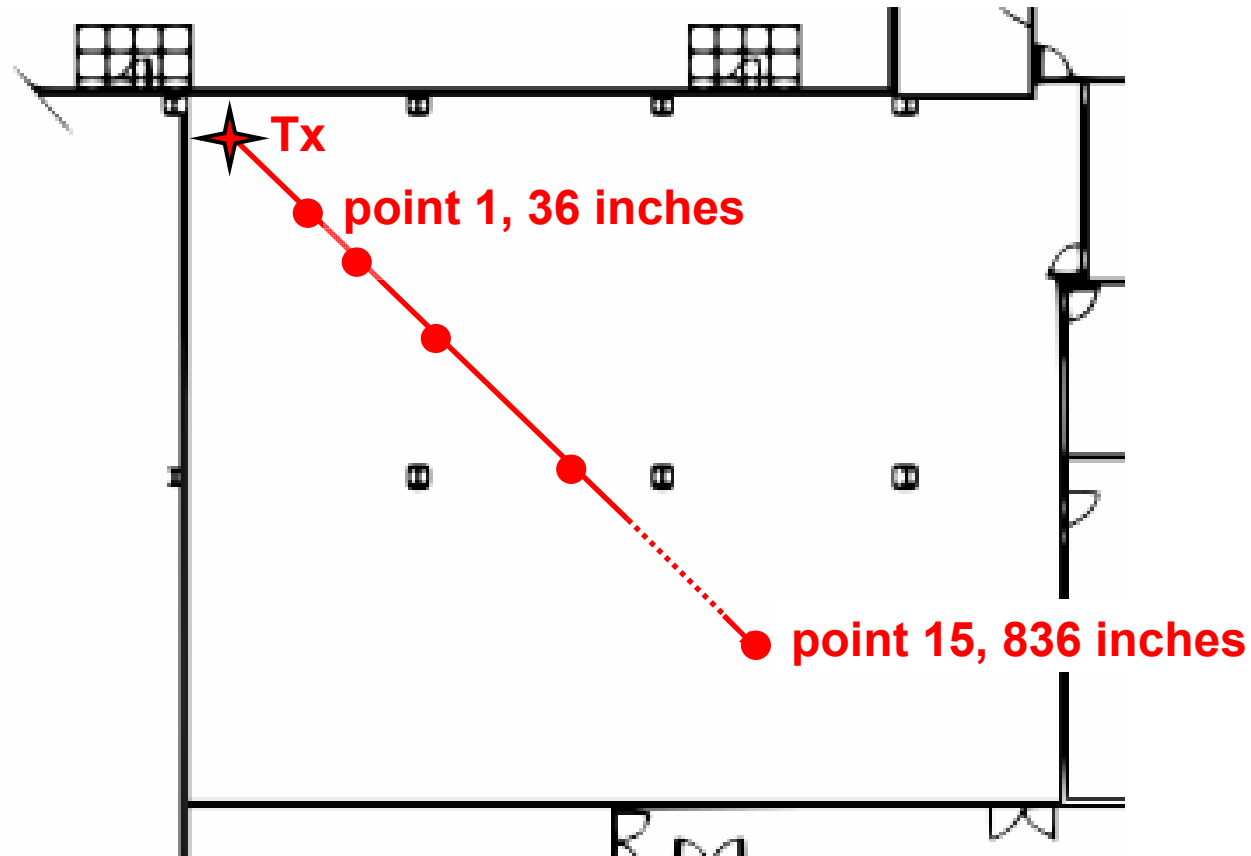
- $p^k(\tau)$ **spatial** average in the radius of a few wavelengths

- Multipath intensity profile (MIP)

- $p^k(\tau)$ **time** average at a spot k (“local PDP”)
- we measure MIP
 - ORBIT nodes in the room are static
 - ORBIT experiments utilize some amount of time

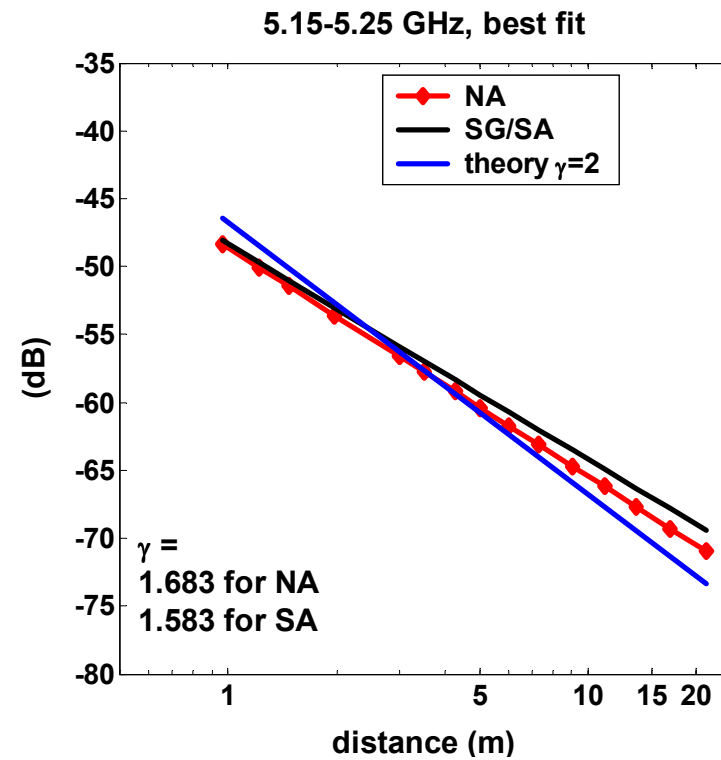
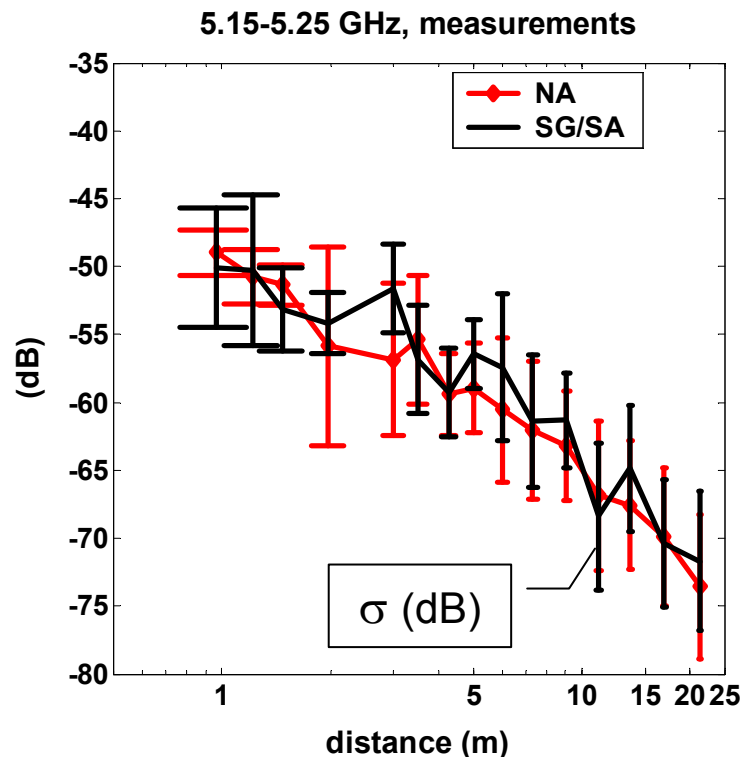
Case study “receiver on a diagonal”

- Logarithmically distributed distances
- Line-of-sight between the antennas



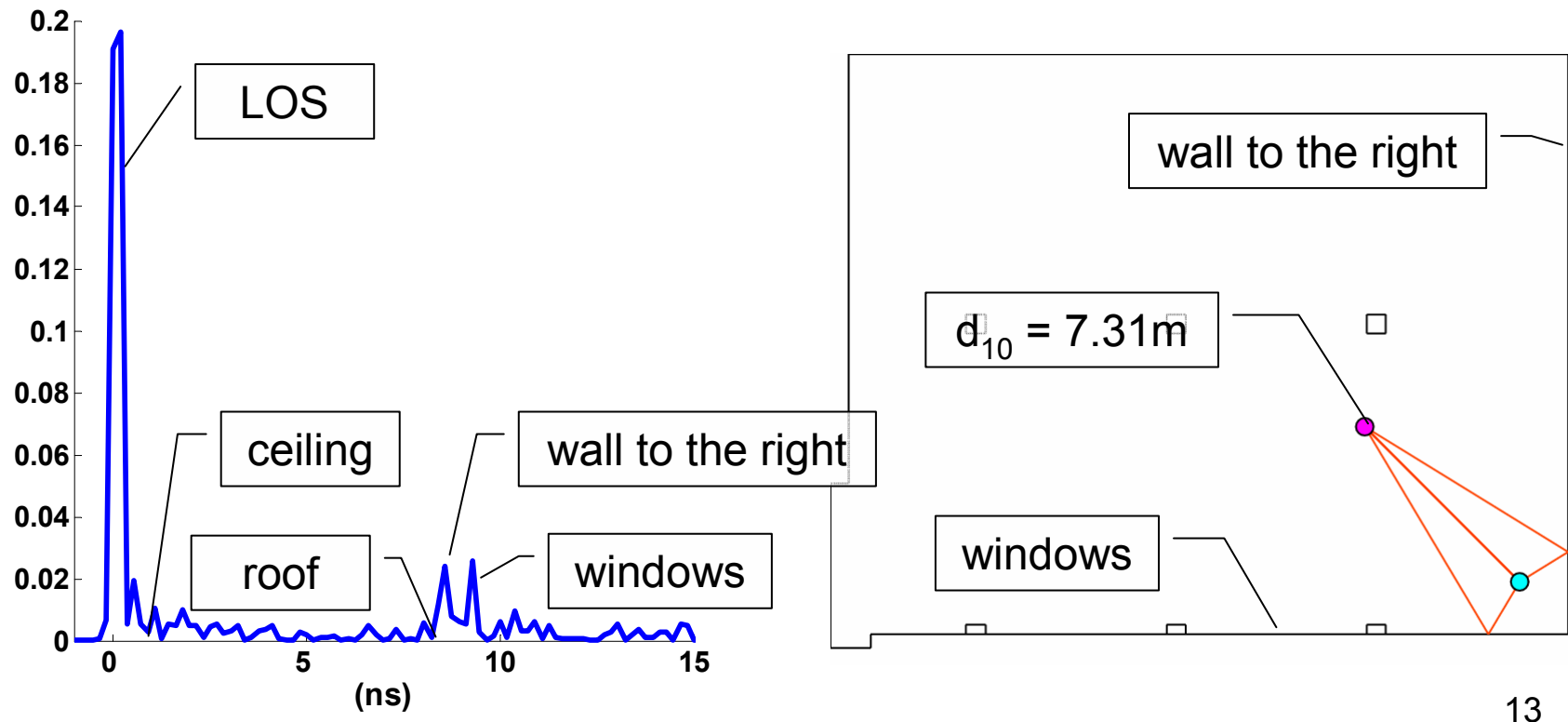
Path loss for receiver on a diagonal

band (GHz)	2.4-2.5	5.15-5.25	5.25-5.35	5.275-5.875	0.4-6
γ^*	1.638	1.683	1.645	1.162	1.730
PL_1^* (dB)	-44.972	-48.335	-49.116	-56.017	-49.592



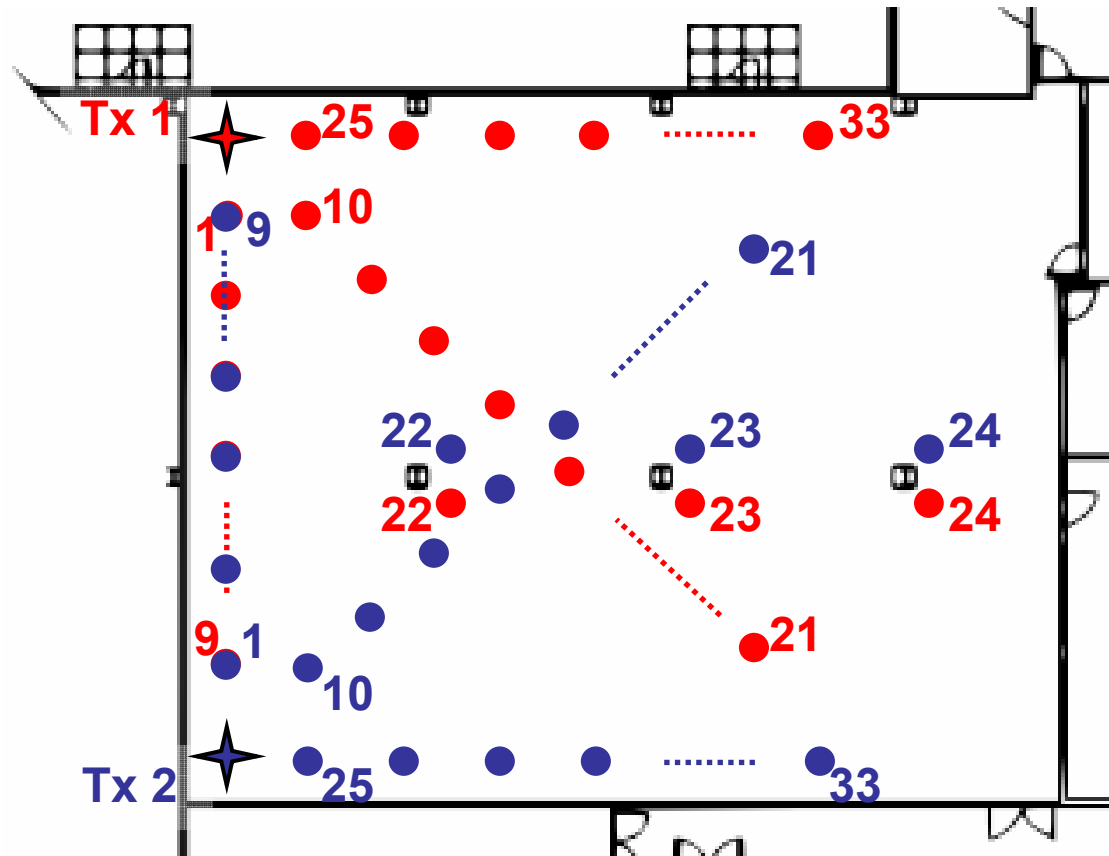
Example of MIP for receiver on a diagonal

- Powers predicted by WISE do not agree with IDFT, but delays do
- Wall, windows significant source of reflections
- Ceiling, roof, floor negligible source of reflections



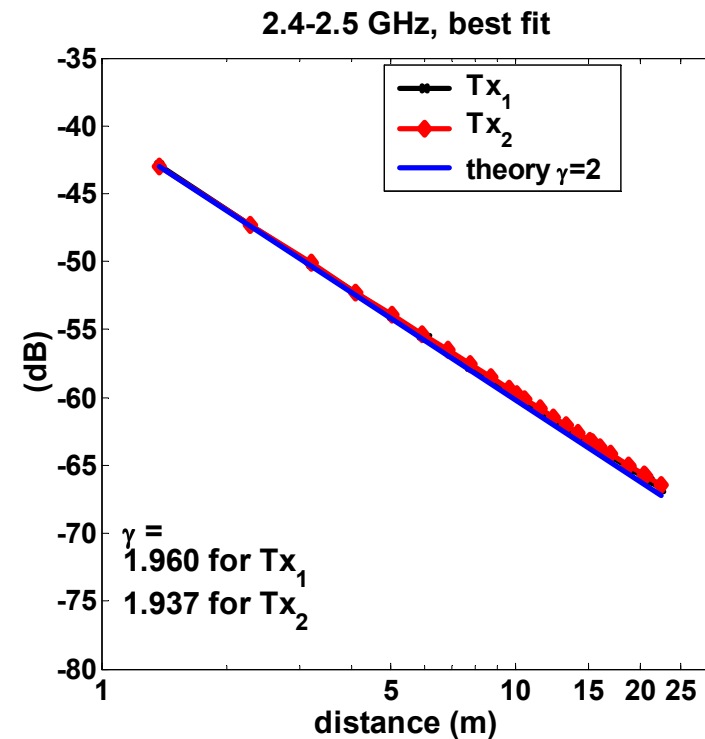
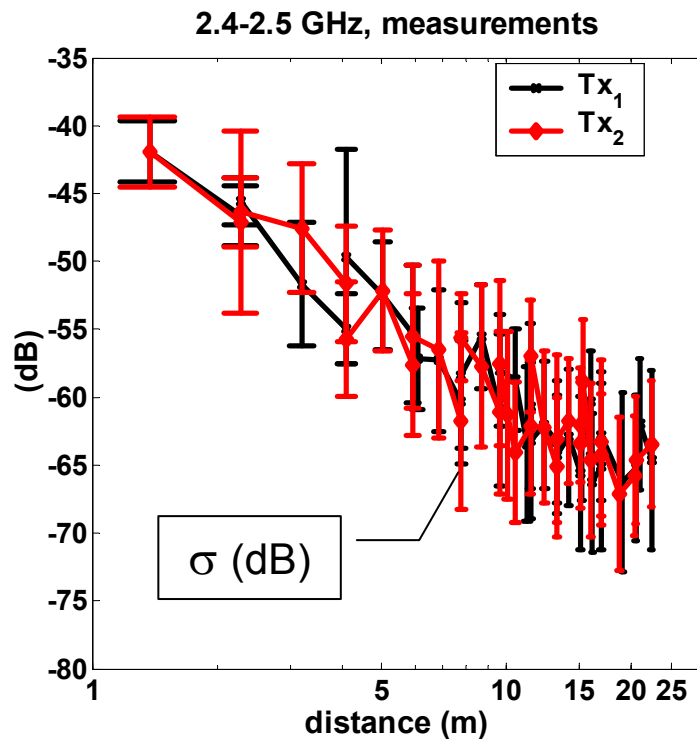
Case study with two transmitter positions

- Distance between measuring points 6 feet
- ORBIT node antennas are obstacles between Tx and Rx



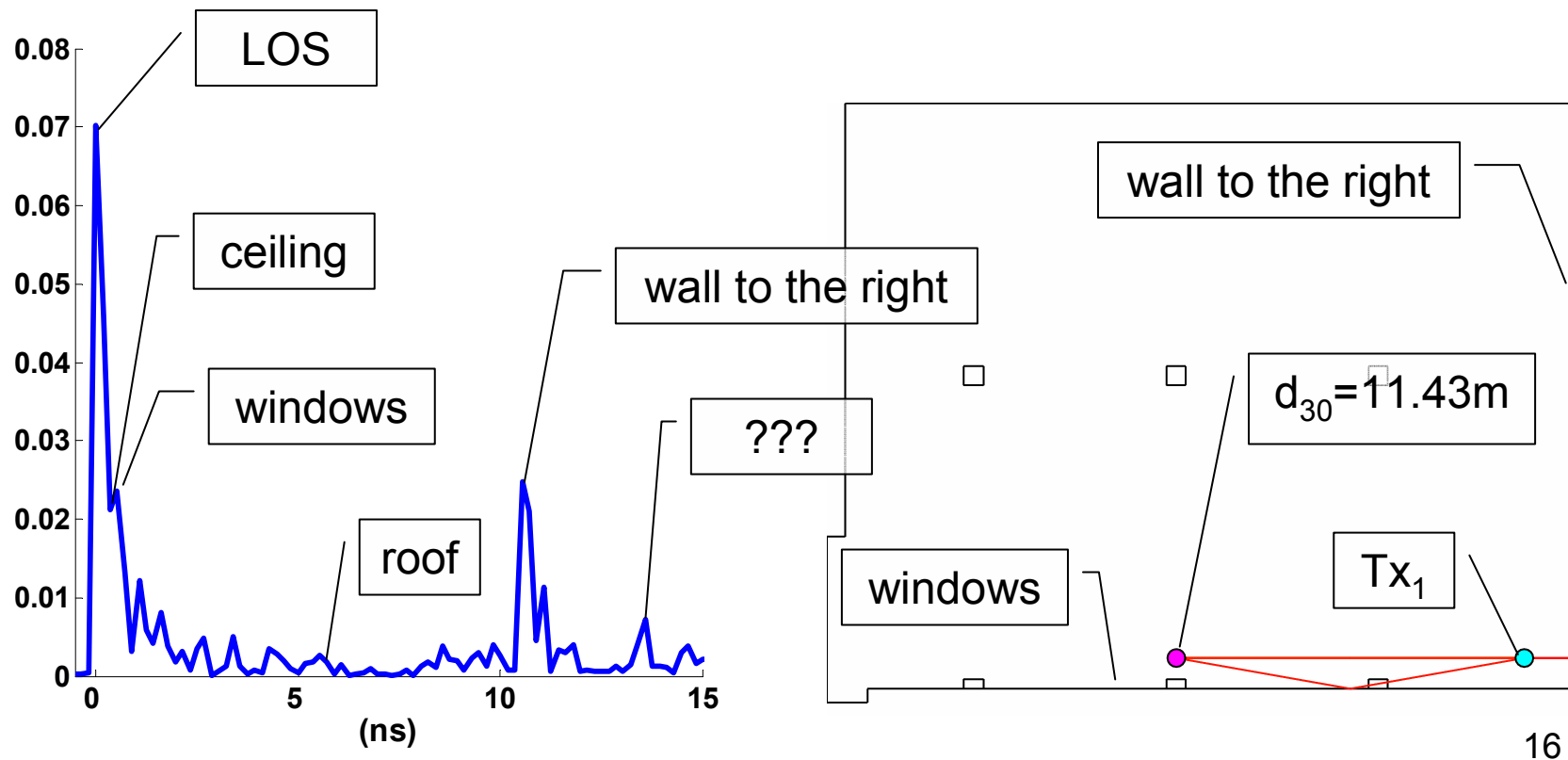
Path loss for two transmitter positions

band (GHz)		2.4-2.5	5.15-5.25	5.25-5.35	5.275-5.875	0.4-6
Tx 1	γ^*	1.960	1.660	1.718	1.732	1.821
	PL_1^* (dB)	-42.934	-54.459	-53.411	-53.398	-50.623
Tx 2	γ^*	1.937	1.701	1.706	1.902	1.833
	PL_1^* (dB)	-42.993	-53.164	-52.805	-50.963	-49.615



Example of MIP for two transmitter positions

- Again, wall, windows significant source of reflections
- Ceiling, roof, floor negligible source of reflections
- Compared to “diagonal” case a lot of weak reflections



Conclusions

- Path loss coefficient close to 1.8
- Walls are significant source of reflections
- Reflections from ceiling, floor, and roof are negligible